



## 1.0 INPUT

Gantry Girder Span  $L_G = 7500$  mm

### 1.1 Section Shape

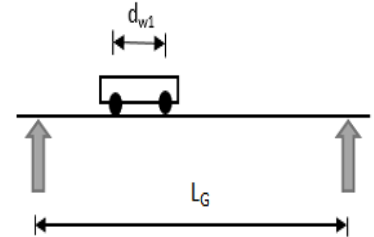
Type = **Rolled I Section + Plate**

I Section = **UB 610x305x179**

#### 1.1.1 Top Plate

Width of Plate  $b_p = 350$  mm

Thickness of Plate  $t_p = 30$  mm



### 1.2 Wheel Arrangement

No of Wheels Per End Carriage  $N_w = 2$

Distance of End Carriage Wheel Centers  $d_{w1} = 4000$  mm

Crane Rail Height  $h_r = 100$  mm



### 1.3 Restraints

Destabilizing = **Yes**

Restraint Condition = **Compression Flange  
Laterally Restrained  
Both Flanges Fully  
Restrained**

Span Type = **Interior Span**

### 1.4 Loads (Unfactored)

User Defined Wheel Load = **Yes**

Static Wheel Load  $W_{stat} = 100$  kN

Transverse Surge Load Per Wheel  $W_{su} = 10$  %

Dynamic Wheel Load Factor  $W_{dy} = 1.5$

Unfactored Weight of Crane Rail  $W_r = 0.5$  kN/m

### 1.5 Weld

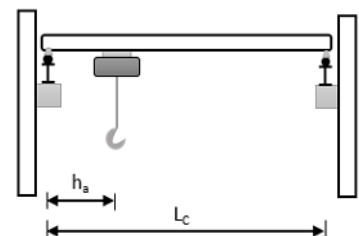
Type = **Continuous**

Weld Length  $S = 5$  mm

### 1.6 Deflection

Vertical Deflection Limit  $\delta_{av} = 600$

Horizontal Deflection Limit  $\delta_{ah} = 500$



### 1.7 Properties

Modulus of Elasticity  $E = 205000$  N/mm<sup>2</sup>

Class of Crane  $C_c = Q3$

Steel Grade  $f_y = 460$  N/mm<sup>2</sup>

## 2.1 Effective Length

Restraint Condition Factor	$L_E$	=	<b>0.85</b>
Effective Length of Gantry Girder	$L_g$	=	$L_E * L_G = \mathbf{6.38}$ m

Table 13

## 2.2 Section Properties

## 2.2.1 I Section [From Section Table]

Section Mass	$Mass_{bm}$	=	<b>179</b> kg/m
Cross Sectional Area	$A_{bm}$	=	<b>228</b> cm <sup>2</sup>
Overall Depth of Section	$D_{bm}$	=	<b>620.2</b> mm
Breadth of Section	$B_{bm}$	=	<b>307.1</b> mm
Web Thickness	$t_{bm}$	=	<b>14.1</b> mm
Flange Thickness	$T_{bm}$	=	<b>23.6</b> mm
Root Radius	$r_{bm}$	=	<b>16.5</b> mm
Depth of Web	$d_{bm}$	=	<b>540</b> mm
End Clearance	$C_{bm}$	=	<b>9.05</b> mm
Moment of Inertia - Major	$I_{xxbm}$	=	<b>153000</b> cm <sup>4</sup>
Moment of Inertia - Minor	$I_{yybm}$	=	<b>11400</b> cm <sup>4</sup>
Radius of Gyration - Major	$r_{xxbm}$	=	<b>25.9</b> cm
Radius of Gyration - Minor	$r_{yybm}$	=	<b>7.07</b> cm
Elastic Section Modulus - Major	$Z_{xxbm}$	=	<b>4930</b> cm <sup>3</sup>
Elastic Section Modulus - Minor	$Z_{yybm}$	=	<b>743</b> cm <sup>3</sup>
Plastic Section Modulus - Major	$S_{xxbm}$	=	<b>5550</b> cm <sup>3</sup>
Plastic Section Modulus - Minor	$S_{yybm}$	=	<b>1140</b> cm <sup>3</sup>
Warping Constant	$H_{bm}$	=	<b>10.2</b> dm <sup>6</sup>
Buckling Parameter	$u_{bm}$	=	<b>0.886</b>
Torsional Index	$x_{bm}$	=	<b>27.7</b>
Torsion Constant	$J_{bm}$	=	<b>340</b> cm <sup>4</sup>

## 2.2.2 Plate

Area of Plate	$A_{pl}$	=	$b_p * t_p = \mathbf{105}$ cm <sup>2</sup>
Mass of Plate	$Mass_{pl}$	=	$b_p * t_p * 7850 = \mathbf{82.4}$ kg/m
Moment of Inertia - Major	$I_{xxpl}$	=	$t_p * b_p^3 / 12 = \mathbf{10718.8}$ cm <sup>4</sup>
Moment of Inertia - Minor	$I_{yypl}$	=	$b_p * t_p^3 / 12 = \mathbf{78.8}$ cm <sup>4</sup>
Torsion Constant	$J_{pl}$	=	$b_p * t_p^3 / 3 = \mathbf{315}$ cm <sup>4</sup>

## 2.2.3 Elastic Section Properties (I + Plate)

Position of Neutral Axis Above Bottom Flange	$Y_{nap}$	=	$((A_{bm} * D_{bm} / 2) + (A_{pl} * (D_{bm} + 0.5) * t_p)) /$ $(A_{bm} + A_{pl}) = \mathbf{412.6}$ mm
Moment of Inertia About Major Axis	$I_{xxp}$	=	$I_{xxbm} + (A_{bm} * (Y_{nap} - (D_{bm} / 2))^2) + I_{yypl} + (A_{pl} * (D_{bm} + 0.5 * t_p - Y_{nap})^2) = \mathbf{229061.3}$ cm <sup>4</sup>
Moment of Inertia About Minor Axis	$I_{yyp}$	=	$I_{yybm} + I_{xxpl} = \mathbf{22118.8}$ cm <sup>4</sup>
Elastic Modulus About Major Axis (Top)	$Z_{xxtopp}$	=	$I_{xxp} / (D_{bm} + t_p - Y_{nap}) = \mathbf{9641}$ cm <sup>3</sup>
Elastic Modulus About Major Axis (Bottom)	$Z_{xxbtmp}$	=	$I_{xxp} / Y_{nap} = \mathbf{5551.5}$ cm <sup>3</sup>
Elastic Modulus About Minor Axis	$Z_{yyp}$	=	$I_{yyp} / (b_p / 2) = \mathbf{1263.9}$ cm <sup>3</sup>
Radius of Gyration	$r_{yp}$	=	$(I_{yyp} / (A_{bm} + A_{pl}))^{0.5} = \mathbf{81.5}$ mm

Area of Beam Flange	$A_{flp} = T_{bm} * B_{bm} = \mathbf{7247.6 \text{ mm}^2}$
Position of Equal Area Axis (E.A.A)	$Y_{eap} = T_{bm} + (((A_{bm} + A_{pl}) / 2) - A_{flp}) / t_{bm} = \mathbf{600.9 \text{ mm}}$

### 2.2.4 Plastic Section Properties (I + Plate)

Plate Component Above E.A.A	$S_{xupl} = A_{pl} * (D_{bm} + t_p * 0.5 - Y_{eap}) = \mathbf{360.1 \text{ cm}^3}$
Plate Component Below E.A.A	$S_{xipl} = \mathbf{0 \text{ cm}^3}$
Top Flange Component Above E.A.A	$S_{xutfl} = B_{bm} * (D_{bm} - Y_{eap})^2 / 2 = \mathbf{57.1 \text{ cm}^3}$
Top Flange Component Below E.A.A	$S_{xltfl} = B_{bm} * (Y_{eap} - (D_{bm} - T_{bm}))^2 / 2 = \mathbf{2.9 \text{ cm}^3}$
Beam Web Component Above E.A.A	$S_{xuweb} = \mathbf{0 \text{ cm}^3}$
Beam Web Component Below E.A.A	$S_{xlweb} = t_{bm} * (D_{bm} - (2 * T_{bm})) * (Y_{eap} - T_{bm} - (D_{bm} - 2 * T_{bm}) / 2) = \mathbf{2349.5 \text{ cm}^3}$
Beam Bottom Flange Component	$S_{xbfl} = A_{flp} * (Y_{eap} - 0.5 * T_{bm}) = \mathbf{4269.6 \text{ cm}^3}$
Plastic Section Modulus About Major Axis	$S_{xp} = S_{xupl} + S_{xipl} + S_{xutfl} + S_{xltfl} + S_{xuweb} + S_{xlweb} + S_{xbfl} = \mathbf{7039.2 \text{ cm}^3}$

### 2.2.5 Torsional Index (I + Plate)

Annex. B.2.4.1

Combined Torsional Constant	$J_p = J_{bm} + J_{pl} = \mathbf{655 \text{ cm}^4}$
Position of Top Shear Center from Top Section	$S_{ctp} = ((A_{pl} * 0.5 * t_p) + (A_{flp} * (t_p + 0.5 * T_{bm}))) / (A_{pl} + A_{flp}) = \mathbf{25.9 \text{ mm}}$
Distance Between Flange Shear Centers	$h_{sp} = D_{bm} + t_p - 0.5 * T_{bm} - S_{ctp} = \mathbf{612.5 \text{ mm}}$
Torsional Index	$x_p = 0.566 * h_{sp} * ((A_{bm} + A_{pl}) / J_p)^{0.5} = \mathbf{24.7}$
Buckling Parameter	$u = ((4 * S_{xp}^2 * (1 - (I_{yyp} / I_{xyp}))) / ((A_{bm} + A_{pl})^2 * h_{sp}^2))^{0.25} = \mathbf{0.8}$

Annex. B.2.3

### 2.2.6 Flange Ratio / Mono Symmetry Index

Cl. 4.3.6.7

Inertia of Top Flange (Major)	$I_{tfp} = I_{xpl} + (T_{bm} * B_{bm}^3 / 12) = \mathbf{16414.8 \text{ cm}^4}$
Inertia of Top Flange (Minor)	$I_{bfp} = T_{bm} * B_{bm}^3 / 12 = \mathbf{5696 \text{ cm}^4}$
Flange Ratio	$\eta_{sagp} = I_{tfp} / (I_{tfp} + I_{bfp}) = \mathbf{0.742}$
Mono Symmetry Index	$\psi_{sagp} = 0.8 * ((2 * \eta_{sagp}) - 1) = \mathbf{0.388}$

### 2.2.7 Top Flange Properties (Top Flange of I Section + Plate)

Elastic Modulus	$Z_{tfp} = I_{tfp} / (b_p / 2) = \mathbf{938 \text{ cm}^3}$
Plastic Modulus	$S_{tfp} = t_p * b_p^2 / 4 + (T_{bm} * B_{bm}^2 / 4) = \mathbf{1475.2 \text{ cm}^3}$

## 2.3 Section Classification

Table 11

Maximum Steel Thickness	$t_{max} = \max(T_{bm}, t_p) = \mathbf{30 \text{ mm}}$
Steel Design Strength	$p_y = \mathbf{440 \text{ N/mm}^2}$
Ratio	$\epsilon = (275 / p_y)^{0.5} = \mathbf{0.791}$
Plate Outstand (Outstand Element)	$R_{ratio1} = (0.5 * b_p - 0.5 * B_{bm}) / t_p = \mathbf{0.715}$
Inner Plate (Internal Element)	$R_{ratio2} = B_{bm} / t_p = \mathbf{10.237}$
Beam Flange	$R_{ratio3} = b_p / (2 * T_{bm}) = \mathbf{7.415}$
Beam Web	$R_{ratio4} = d_{bm} / t_{bm} = \mathbf{38.298}$
Flange Classification	= <b>Compact</b> ( $9\epsilon < \text{Flange} \leq 10\epsilon$ )
Web Classification	= <b>Plastic</b> ( $\text{Web} < 80\epsilon$ )
Overall Section Classification	= <b>Compact</b>

Table 9

## 2.4 Section Capacity Calculation

### 2.4.1 Shear Capacity

Cl. 4.2.3

Vertical Shear Capacity	$P_{wp} = 0.6 * p_y * t_{bm} * D_{bm} = \mathbf{2308.6 \text{ kN}}$
Horizontal Shear Capacity of Beam Flange	$P_{vhbmp} = 0.6 * p_y * 0.9 * T_{bm} * B_{bm} = \mathbf{1722 \text{ kN}}$

Horizontal Shear Capacity of Plate  $P_{vhlp} = 0.6 * p_y * 0.9 * t_p * b_p = \mathbf{2494.8 \text{ kN}}$   
 Combined Horizontal Shear Capacity  $P_{vhp} = P_{vhbmp} + P_{vhlp} = \mathbf{4216.8 \text{ kN}}$

### 2.4.2 Bending Capacity

Cl. 4.2.5

Vertical Bending Capacity  $M_{cxp} = \min(p_y * S_{xp}, 1.2 * p_y * \min(Z_{xxtopp}, Z_{xxbtm})) = \mathbf{2931.2 \text{ kNm}}$   
 Horizontal Moment Capacity Top Flange  $M_{ctfp} = \min(p_y * S_{tfp}, 1.2 * p_y * Z_{tfp}) = \mathbf{495.3 \text{ kNm}}$

### 2.4.3 Lateral Torsional Buckling Capacity

Slenderness Ratio  $\lambda_p = L_g / r_{yp} = \mathbf{78.221}$   
 Slenderness Factor  $v_p = 1 / (((4 * \eta_{sagp} * (1 - \eta_{sagp})) + (0.05 * (\lambda_p / x_p)^2) + \psi_{sagp}^2)^{0.5} + \psi_{sagp})^{0.5} = \mathbf{0.796}$  *Annex. B.2.3*  
 Factor  $\beta_{wp} = \min(Z_{xxtopp}, Z_{xxbtm}) / S_{xp} = \mathbf{1}$  *Cl. 4.3.6.9*  
 Equivalent Slenderness  $\lambda_{ltp} = u * v_p * \lambda_p * \beta_{wp}^{0.5} = \mathbf{50.441}$   
 Limiting Equivalent Slenderness  $\lambda_{lop} = 0.4 * (\pi^2 * E / p_y)^{0.5} = \mathbf{27.124}$   
 Perry Factor  $\eta_{ltp} = 0.014 * (\lambda_{ltp} - \lambda_{lop}) = \mathbf{0.326}$  *Annex. B.2.2*  
 Euler Buckling Stress  $p_{ep} = (\pi^2 * E) / \lambda_{lt}^2 = \mathbf{795.2 \text{ N/mm}^2}$   
 Factor  $\phi_{Ltp} = (p_y + ((\eta_{ltp} + 1) * p_{ep})) / 2 = \mathbf{747.4 \text{ N/mm}^2}$  *Annex. B.2.1*  
 Bending Strength  $p_{bp} = p_{ep} * p_y / (\phi_{Ltp}^2 + (\phi_{Ltp}^2 - (p_{ep} * p_y))^{0.5}) = \mathbf{290.6 \text{ N/mm}^2}$   
 Buckling Moment Resistance  $M_{ballow} = p_{bp} * S_{xp} = \mathbf{2045.2 \text{ kNm}}$

## 2.5 Load Calculations

### 2.5.1 Load Case

- W.L - Dynamic Wheel Load
- S.W - Self Weight of Gantry
- S - Surge Wheel Load
- C - Crabbing Wheel Load

### 2.5.2 Weight of Girder

Beam and Crane Rail Self Weight (S.W)  $W_{sw} = (\text{Mass}_{bm} + \text{Mass}_{pl}) * g + W_r = \mathbf{3.06 \text{ kN/m}}$

### 2.5.3 Dynamic Loads Per Wheel

Unfactored Transverse Surge Wheel Load (S)  $W_{sur} = W_{su} * W_{stat} = \mathbf{10 \text{ kN}}$   
 Max. Unfactored Dynamic Vertical Load (W.L)  $W_{dyn} = W_{dy} * W_{stat} = \mathbf{150 \text{ kN}}$   
 Unfactored Transverse Crabbing Load (C)  $W_{cra} = W_{dyn} / 20 = \mathbf{7.5 \text{ kN}}$

### 2.5.4 Load Combination

- L.C. 01 - 1.6 x W.L + 1.4 x S.W
- L.C. 02 - 1.4 x W.L + 1.4 x S.W + 1.4 x S + 1.4 x C

## 2.6 Analysis and Design

### 2.6.1 Shear

Load Combination	Applied Shear (kN)		Capacity (kN)		Shear Capacity Ratio	
	Vertical (V <sub>v</sub> )	Horizontal (V <sub>h</sub> )	Vertical (V <sub>cv</sub> )	Horizontal (V <sub>ch</sub> )	Vertical (V <sub>v</sub> / V <sub>cv</sub> )	Horizontal (V <sub>h</sub> / V <sub>ch</sub> )
<b>L.C.01</b>	367	-	2308.6	-	0.16	-
<b>L.C.02</b>	367	20.5	2308.6	4216.8	0.16	0.0049

### 2.6.2 Moment

Load Combination	Applied Moment (kNm)		Capacity (kNm)		Interaction Ratio ( $M_v / M_{cv}$ ) + ( $M_h / M_{ch}$ )
	Vertical ( $M_v$ )	Horizontal ( $M_h$ )	Buckling ( $M_{cv}$ )	Horizontal ( $M_{ch}$ )	
<b>L.C.01</b>	510.1	-	2045.2	495.3	0.25
<b>L.C.02</b>	449.6	28.2	2045.2	495.3	0.28

### 2.6.3 Web Bearing

Cl. 4.5.2.1

Stiff Bearing Length Dispersed Through Rail  $b_{1p} = 2 * (h_r + t_p) = \mathbf{260}$  mm

Bearing Capacity of Unstiffened Web  $P_{bw} = (b_{1p} + (5 * (T_{bm} + r_{bm}))) * t_{bm} * p_y = \mathbf{2856.9}$  kN

### 2.6.4 Web Buckling

Cl. 4.5.3.1

Effective Length of Web  $L_{webp} = 1.2 * d_{bm} = \mathbf{648}$  mm

Buckling Capacity of Unstiffened Web  $P_{xr} = 25 * \epsilon * t_{bm} / (b_{1p} + (5 * (T_{bm} + r_{bm}) * d_{bm}))^{0.5}$   
 $* P_{bw} = \mathbf{1596.6}$  kN

### 2.6.5 Check Plate to Beam Flange Weld

Design Weld Strength  $P_{ww} = \mathbf{280}$  N/mm<sup>2</sup>

Table 37

Shear Stress on Weld  $V_w = V_v * A_{pl} * (D_{bm} + 0.5 * t_p - Y_{nap}) / (2 * 0.7 * S * I_{xxp})$   
 $= \mathbf{53.5}$  N/mm<sup>2</sup>

### 2.6.6 Deflection Check

#### 2.6.6.1 Allowable Deflection

Allowable Vertical Deflection  $\delta_{av} = L_G / 600 = \mathbf{12.5}$  mm

Allowable Horizontal Deflection  $\delta_{ah} = L_G / 500 = \mathbf{15}$  mm

#### 2.6.6.2 Actual Deflection

Vertical Deflection  $\delta_v = \mathbf{2.7}$  mm

Horizontal Deflection - due to Surge  $\delta_{hs} = \mathbf{3.4}$  mm

Horizontal Deflection - due to Crab  $\delta_{hc} = \mathbf{2.5}$  mm

Horizontal Deflection  $\delta_h = \max(\delta_{hs}, \delta_{hc}) = \mathbf{3.4}$  mm

## 3.0 SUMMARY

### 3.1 Shear Capacity (kN)

Description	Required	Actual	Status
Vertical	367	2308.6	<b>PASS</b>
Horizontal	20.5	4216.8	<b>PASS</b>

### 3.2 Bending Capacity (kNm)

Description	Required	Actual	Status
Vertical (Buckling)	449.6	2045.2	<b>PASS</b>
Horizontal	28.2	495.3	<b>PASS</b>
Interaction Ratio	1	0.28	<b>PASS</b>

### 3.3 Web Capacity (kN)

Description	Required	Actual	Status
Bearing	240	2856.9	<b>PASS</b>
Buckling	240	1596.6	<b>PASS</b>

Weld Capacity (N/mm <sup>2</sup> )	53.5	280	<b>PASS</b>
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### 3.4 Deflection (mm)

Description	Required	Actual	Status
Vertical	12.5	2.7	<b>PASS</b>
Horizontal	15	3.4	<b>PASS</b>